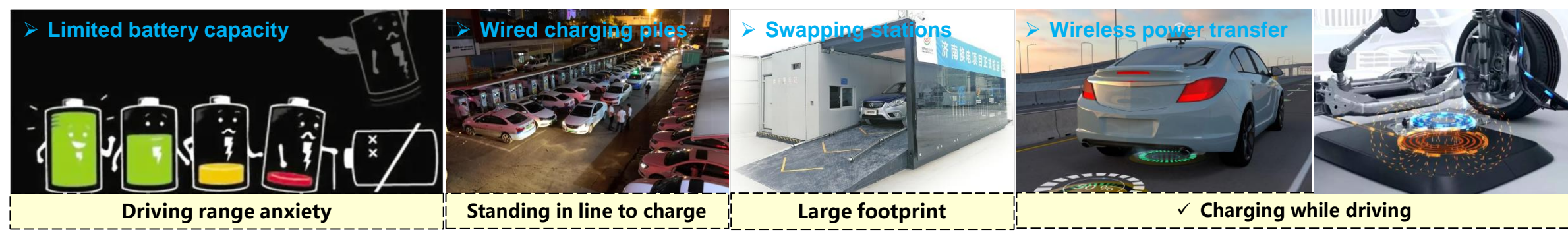
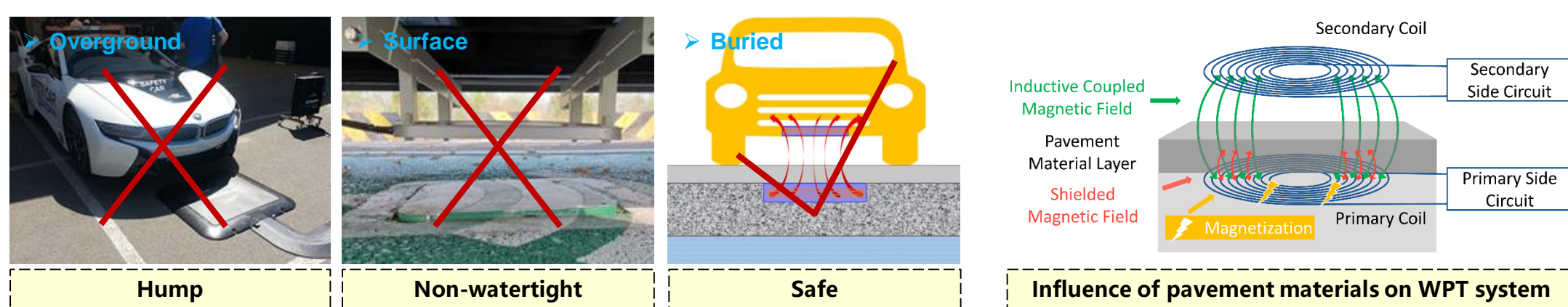


Introduction

- Compared with petrol vehicles, electric vehicles are beneficial to achieving carbon net zero in transportation.
- However, the energy storage capacity of electric vehicle batteries is limited, leading to the driving range anxiety.
- Wireless power transfer (WPT)** technology is considered to be one of the ways to alleviate the charging difficulties.



- In practice, to ensure the durability of pavement, and prevent the circuits to become obstacles for driving, the primary circuits should be buried in the pavement structure.
- Then, the transmission media-air between primary and secondary coil is replaced by pavement materials.
- Previous study indicated that pavement materials can adversely affect the resonant induction coupling process of WPT, reducing the power and efficiency of charging.
- However, the influence mechanism and how to reduce the influence remains unclear.



Objectives

- To quantitatively evaluate the magnetization properties of pavement materials by equivalent magnetic circuit model.
- To evaluate the influence mechanism of pavement materials on the resonant induction coupling process.
- To provide the calculate formulae of resonant frequency for system tuning to reduce the energy loss due to the insertion of pavement materials.

Materials and Modeling

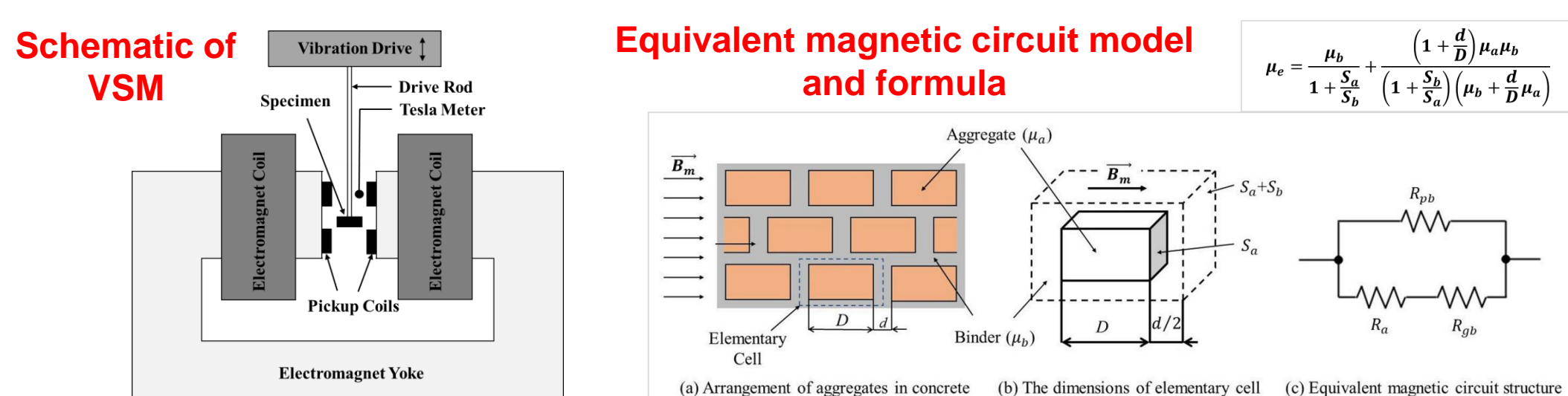
pavement materials

- Asphalt concrete (AC-13 and SMA-13)
- Portland cement concrete (PCC)

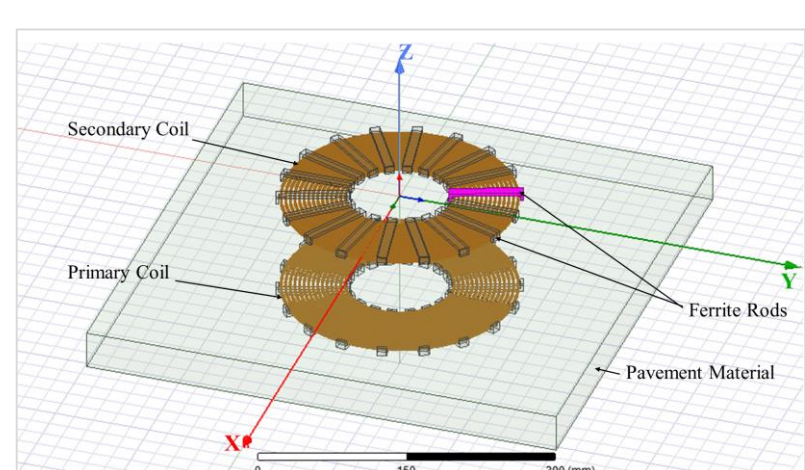


Test of magnetic properties

- Relative permeability of raw materials tested by VSM
- Effective relative permeability** of pavement materials calculated through **equivalent magnetic circuit model**



3D Finite element model and Mathematical model



FEM of resonant induction coupling process to obtain L_1 , L_2 , and M

Calculation formulas of power and efficiency

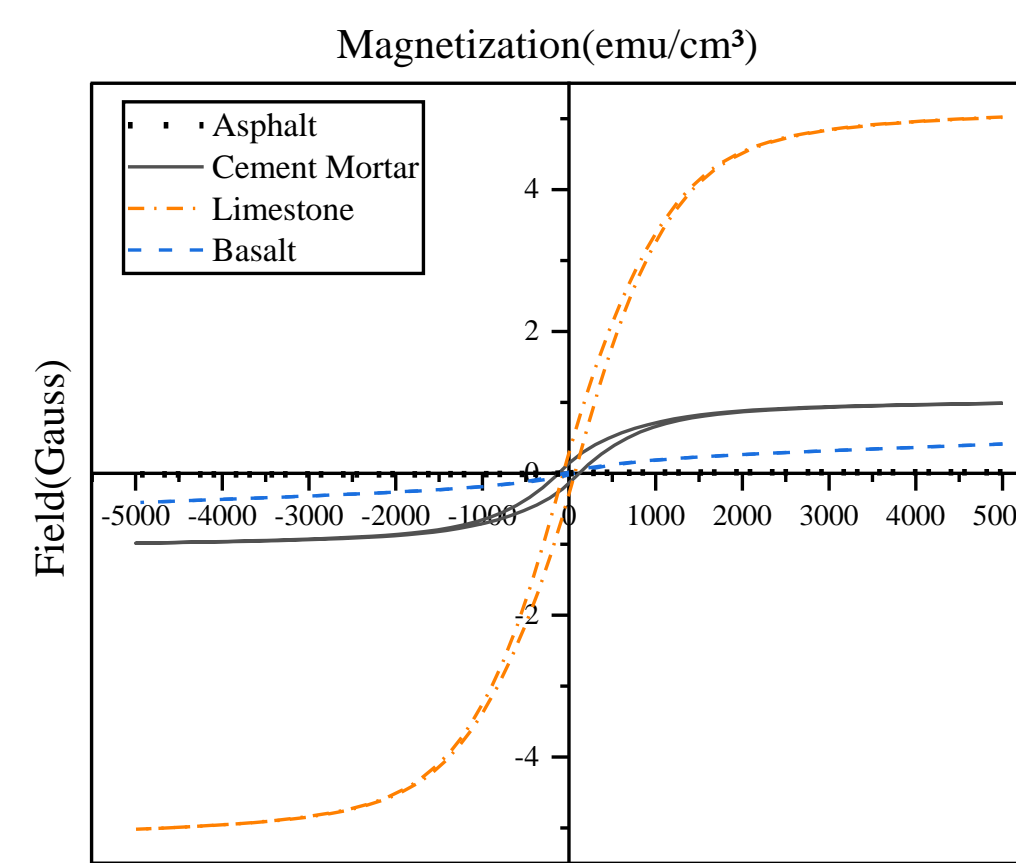
$$\begin{bmatrix} U_1 \\ 0 \end{bmatrix} = \begin{bmatrix} Z_1 & -j\omega M \\ -j\omega M & Z_2 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \quad \omega = \frac{1}{\sqrt{L_1 C_1}} = \frac{1}{\sqrt{L_2 C_2}}$$

$$P_L = I_2^2 R_L = \frac{\omega^2 M^2 U_s^2 R_L}{((R_1 + j(\omega L_1 - \frac{1}{\omega C_1}))(R_2 + j(\omega L_2 - \frac{1}{\omega C_2}) + R_L) + \omega^2 M^2)^2}$$

$$\eta = \frac{R_L}{R_2 + j(\omega L_2 - \frac{1}{\omega C_2}) + R_L} \times \frac{\omega^2 M^2}{(R_1 + j(\omega L_1 - \frac{1}{\omega C_1}))(R_2 + j(\omega L_2 - \frac{1}{\omega C_2}) + R_L) + \omega^2 M^2}$$

Results and discussion

Magnetic properties of pavement materials



Hysteresis loop of raw materials.

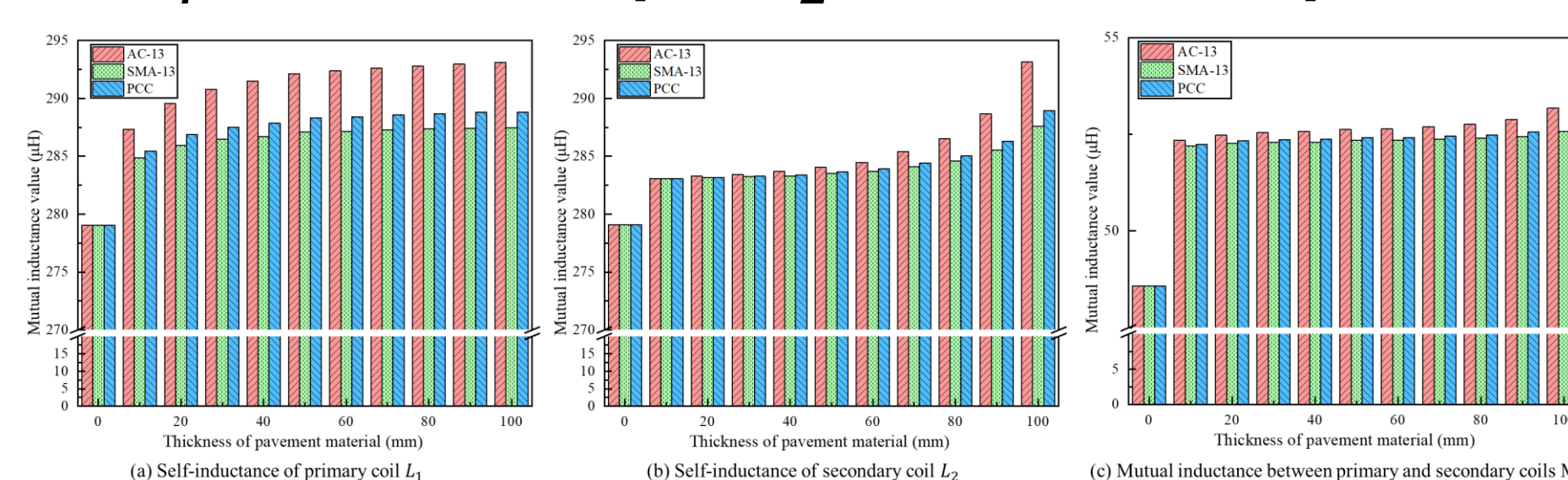
Relative effective permeability of different types of pavement materials

Gradation type	AC-13	SMA-13	PCC
μ_e	1.04864	1.02120	1.02774

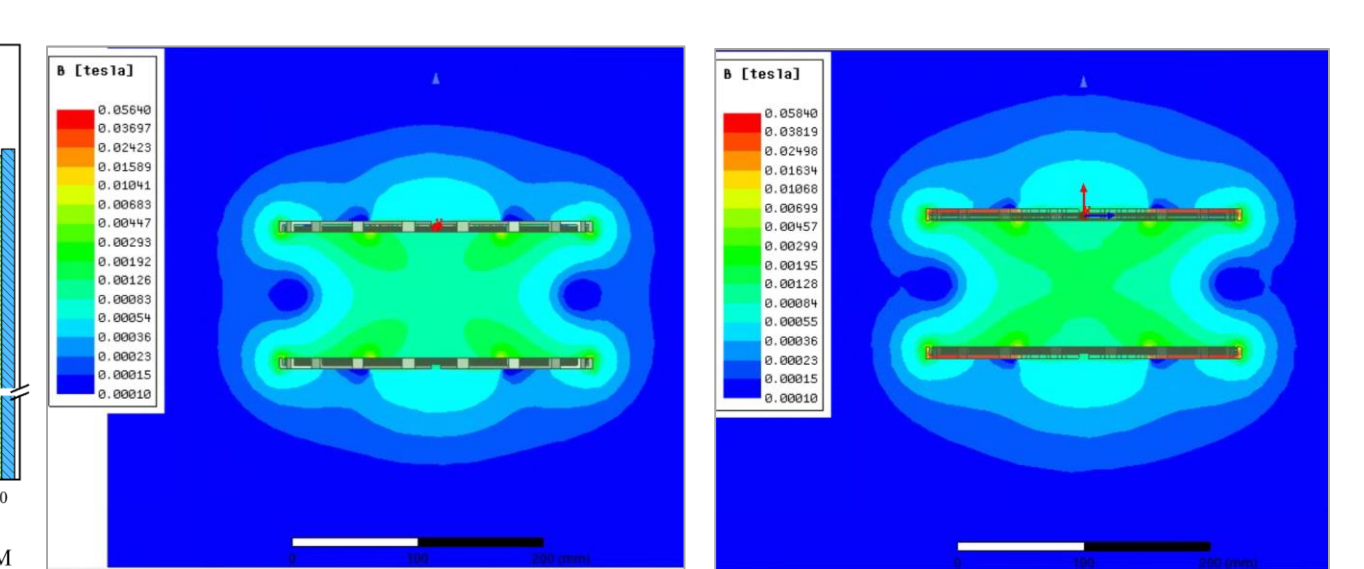
- Among the raw materials, limestone had the highest permeability, followed by cement, basalt was the third, and asphalt had the lowest permeability, which was almost negligible.
- The effective relative permeability of different pavement materials was: **AC-13 > PCC > SMA-13**.

Influence of pavement materials on resonant induction coupling

- L_1 , L_2 , and M increased with the pavement materials inserted because of the increase of magnetic field intensity.
- L_1 : convex shape, L_2 : concave shape, M : first convex, and then concave.



L_1 , L_2 and M at different thicknesses of pavement materials.



Cloud images of magnetic field. (a) AC-0cm. (b) AC-100mm.

Establishment of tuning model

- The thickness factor t_f and material factor a_p^L were constructed according to change rate curves of L_1 , L_2 , and M .
- The tuning formula of resonant induction coupling process was proposed to restore the resonant state.

Tuning formula of WPT

$$t_f = T/TD$$

$$L_{1c} = (a_{p1}^L t_f^3 + b_{p1}^L t_f^2 + c_{p1}^L t_f + d_{p1}^L) L_1$$

$$L_{2c} = (a_{p2}^L t_f^3 + b_{p2}^L t_f^2 + c_{p2}^L t_f + d_{p2}^L) L_2$$

$$M_c = (a_{pM}^L t_f^3 + b_{pM}^L t_f^2 + c_{pM}^L t_f + d_{pM}^L) M$$

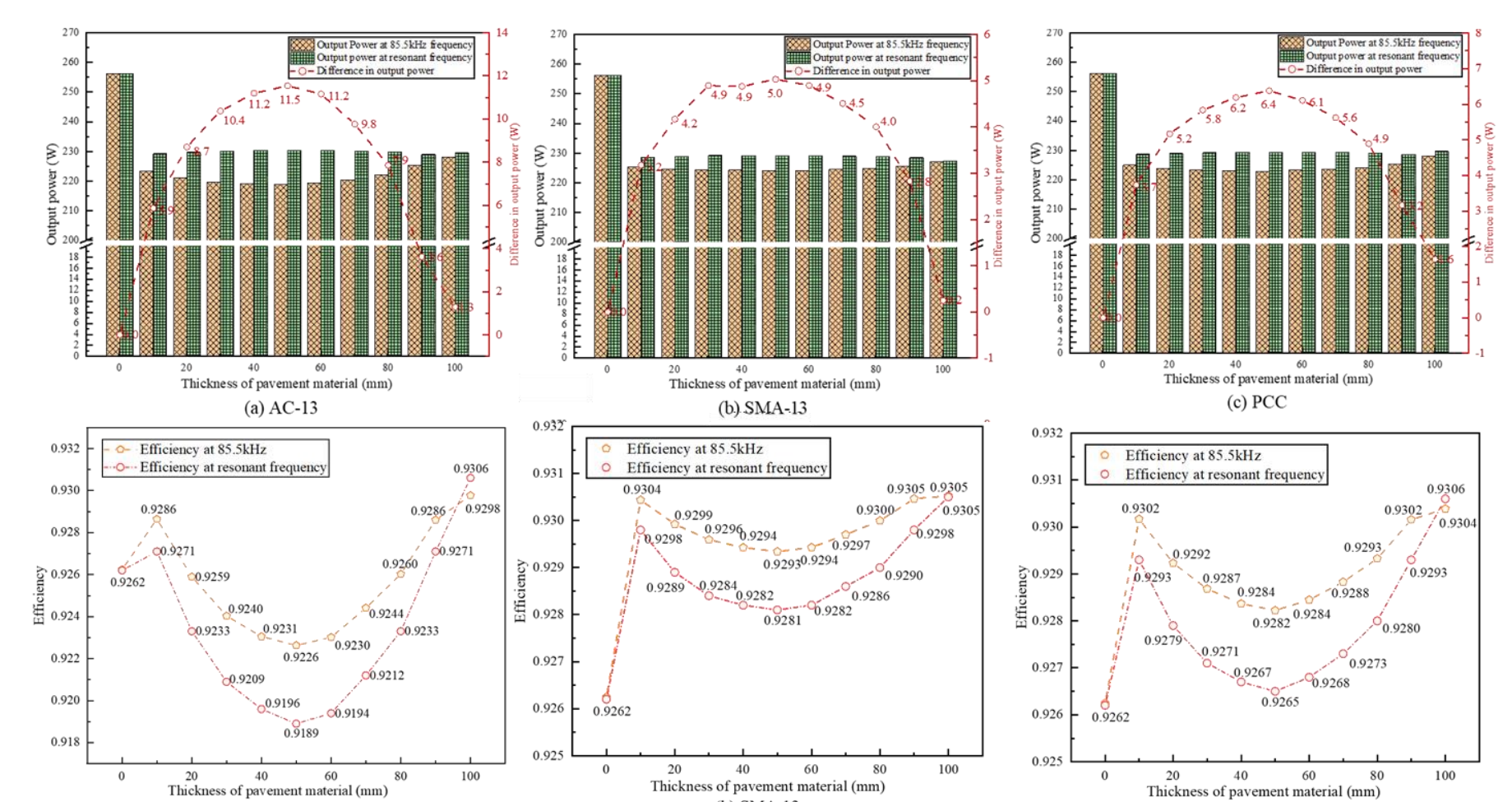
$$\omega_c = \frac{2}{\sqrt{L_{1c} + n^2 L_{2c}} \times \sqrt{C_1 + C_2/n^2}}$$

$$P_{Lc} = I_2^2 R_{Lc} = \frac{4(1 + \frac{C_2}{C_1})(L_{1c} + L_{2c})\omega_c^2 M_c^2 U_s R_L}{((1 + \frac{C_2}{C_1})(L_{1c} + L_{2c})R_1(R_2 + R_L) + 4\omega_c^2 M_c^2)^2}$$

$$\eta_c = \frac{R_L}{R_2 + R_L} \times \frac{4\omega_c^2 M_c^2}{(1 + \frac{C_2}{C_1})(L_{1c} + L_{2c})R_1(R_2 + R_L) + 4\omega_c^2 M_c^2}$$

Verification of tuning model

- After tuning, the output power increased and the efficiency decreased, but the reduction was only about 0.2%.
- The minimum efficiency under the three materials still met the requirements of the specifications.



Output power and efficient of WPT before and after tuning.

Conclusions

- L_1 , L_2 , and M increased with the pavement thickness and the power loss caused by material type was: AC-13 > PCC > SMA-13.
- The loss of power and efficiency can be compensated by adjusting the frequency of the high-frequency voltage supply. The formula for tuning the resonant frequency of the power supply and for calculating the power and efficiency after tuning were given.
- After tuning, the corresponding output power of different kinds of pavement materials from high to low was: AC-13 > PCC > SMA-13. The efficiency of the system before and after tuning was more than 90%, which met the requirements of the specification.
- The tuning model proposed is effective.

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