

Introduction and Objective

Background

- Asphalt materials under **variable vehicle loading amplitudes** exhibit obvious **nonlinear fatigue damage accumulation (NLFDA)** characteristics. However, the **traditional Miner's rule** fails to characterize the NLFDA.

Objective

- Develop an **NLFDA model** to accurately characterize the NLFDA of asphalt binders, and determine the **optimum loading condition of the fatigue life** for asphalt binder.

Materials and Tests

Materials and test conditions

- Materials: SBS modified (SBS) and virgin asphalt binder (VA).
- Equipment: Dynamic shear rheometer (DSR).
- Temperature and frequency: 20°C and 10Hz, respectively.



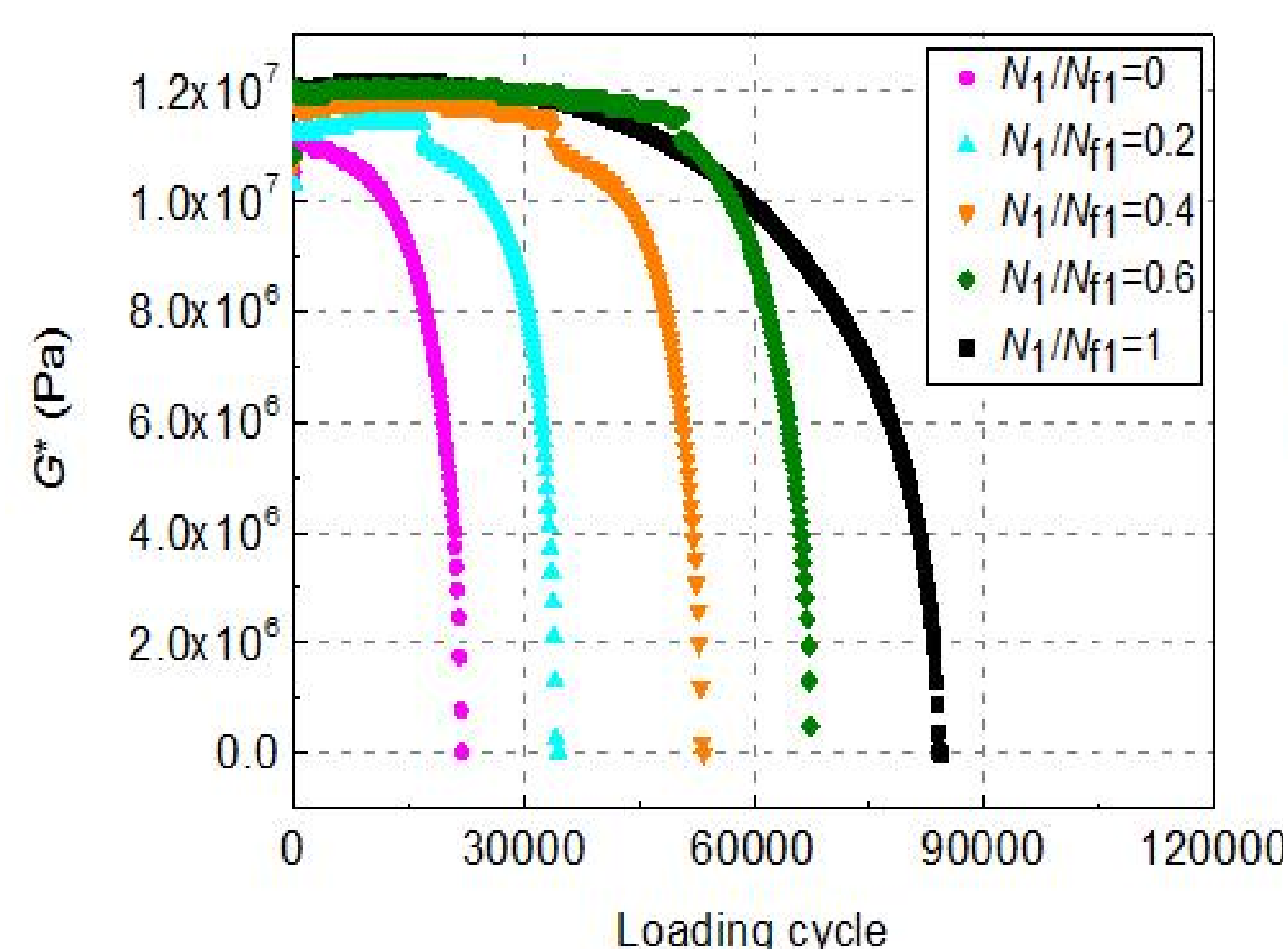
Binder sample DSR

Constant amplitude fatigue test (CAFT)

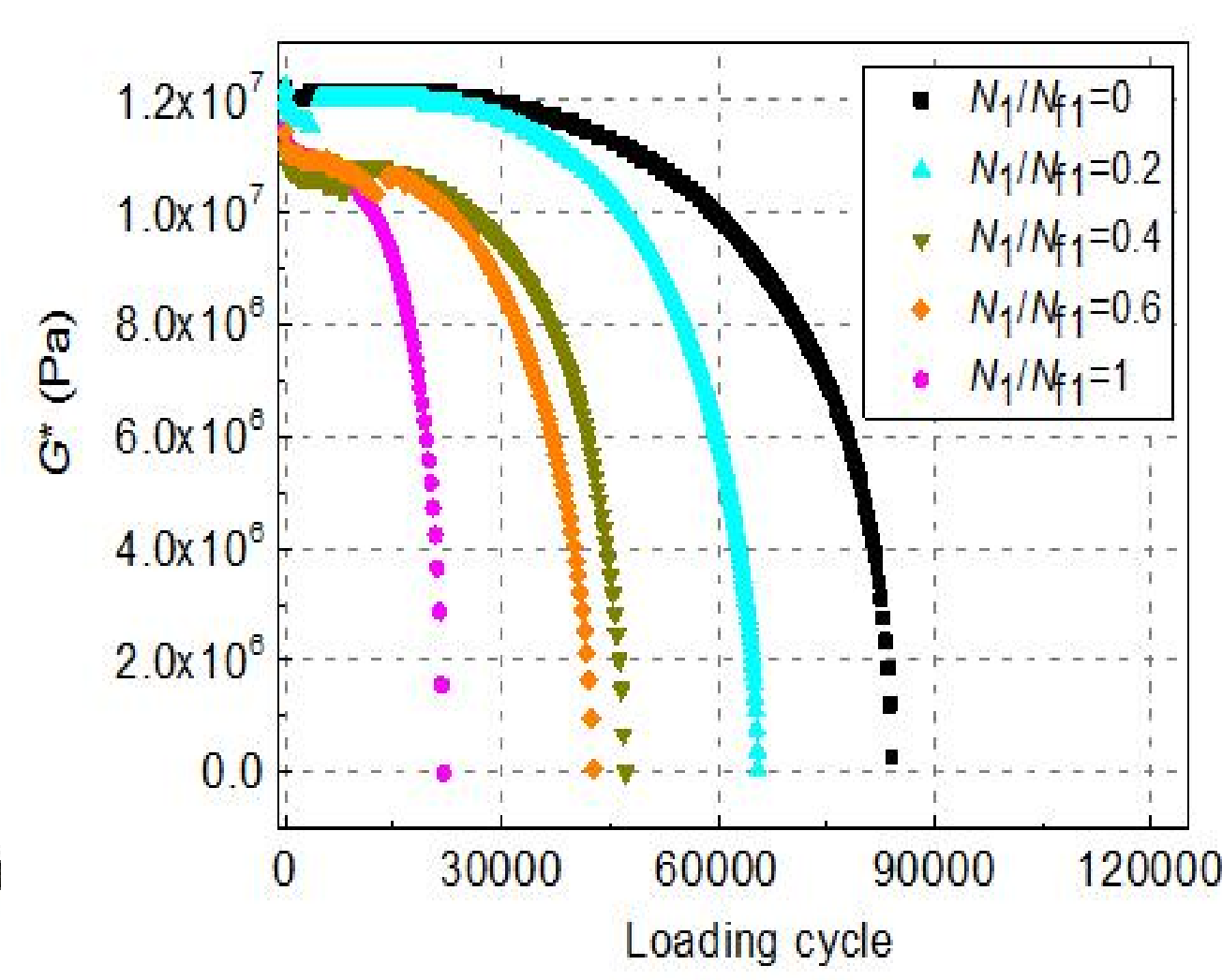
- The high (σ_{high}) and low (σ_{low}) stress levels were applied to the samples, respectively.
- The loading cycle where the shear modulus (G^*) decreases to 0 Pa was defined as the fatigue life (N_f).

Variable amplitude fatigue test (VAFT)

- The first amplitude (σ_1) with the fatigue life of N_{f1} was applied for N_1 cycles corresponding to the N_1/N_{f1} equals to 0, 0.2, 0.4, 0.6 and 1, respectively.
- The second amplitude (σ_2) with the fatigue life of N_{f2} was applied for N_2 cycles.



G^* curves of $\sigma_{low}-\sigma_{high}$ mode



G^* curves of $\sigma_{high}-\sigma_{low}$ mode

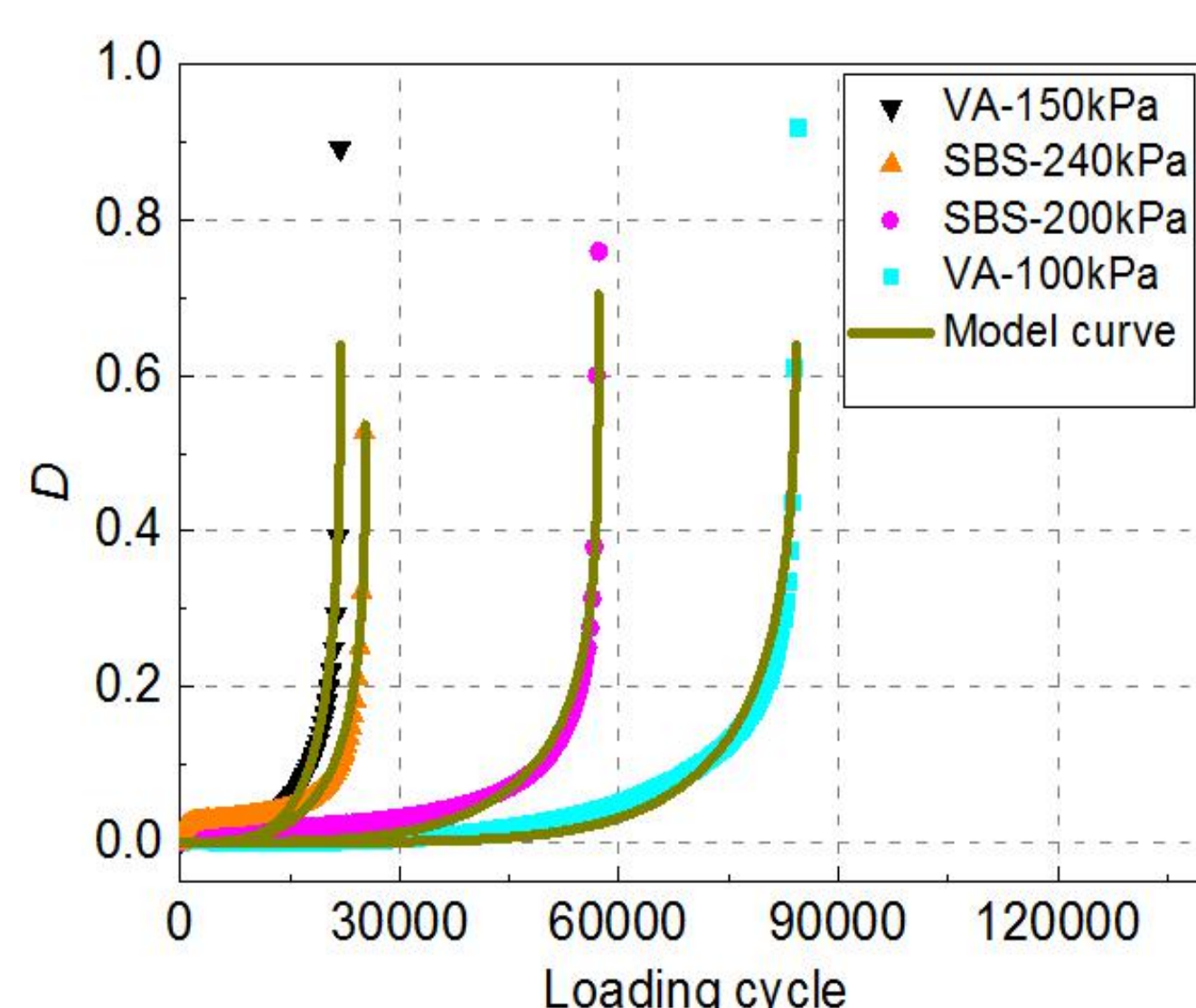
Establishment of NLFDA Model

Damage variable (D)

- The ratio of the **fatigue crack length** of the N th cycle (c) to the maximum crack length (c_{max}) is **defined as the damage variable (D)**.

$$D = c/c_{max} = 1 - (G^{*A}/G^{*T})^{1/4}$$

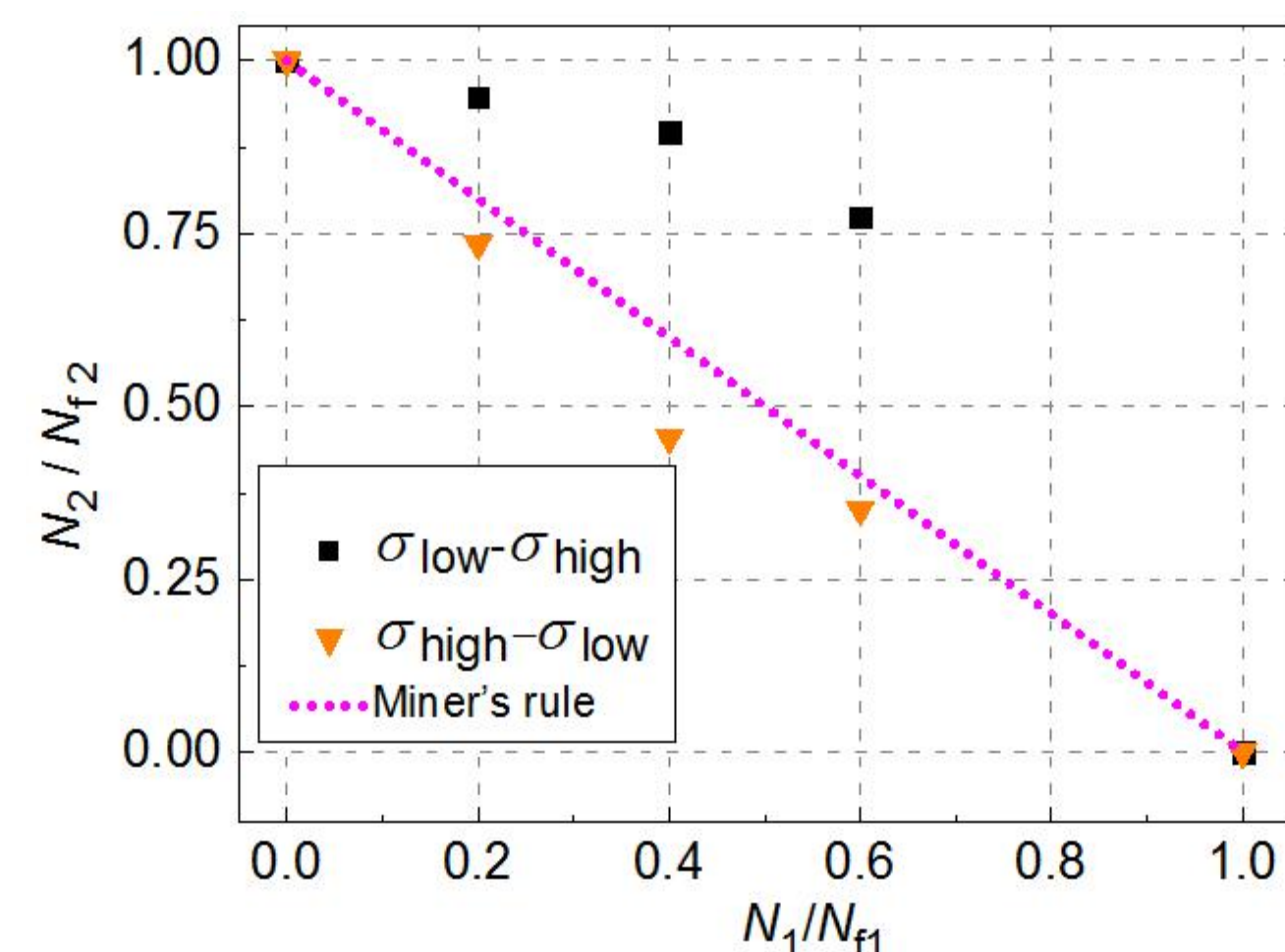
where G^{*A} and G^{*T} are the apparent and true shear modulus, respectively.



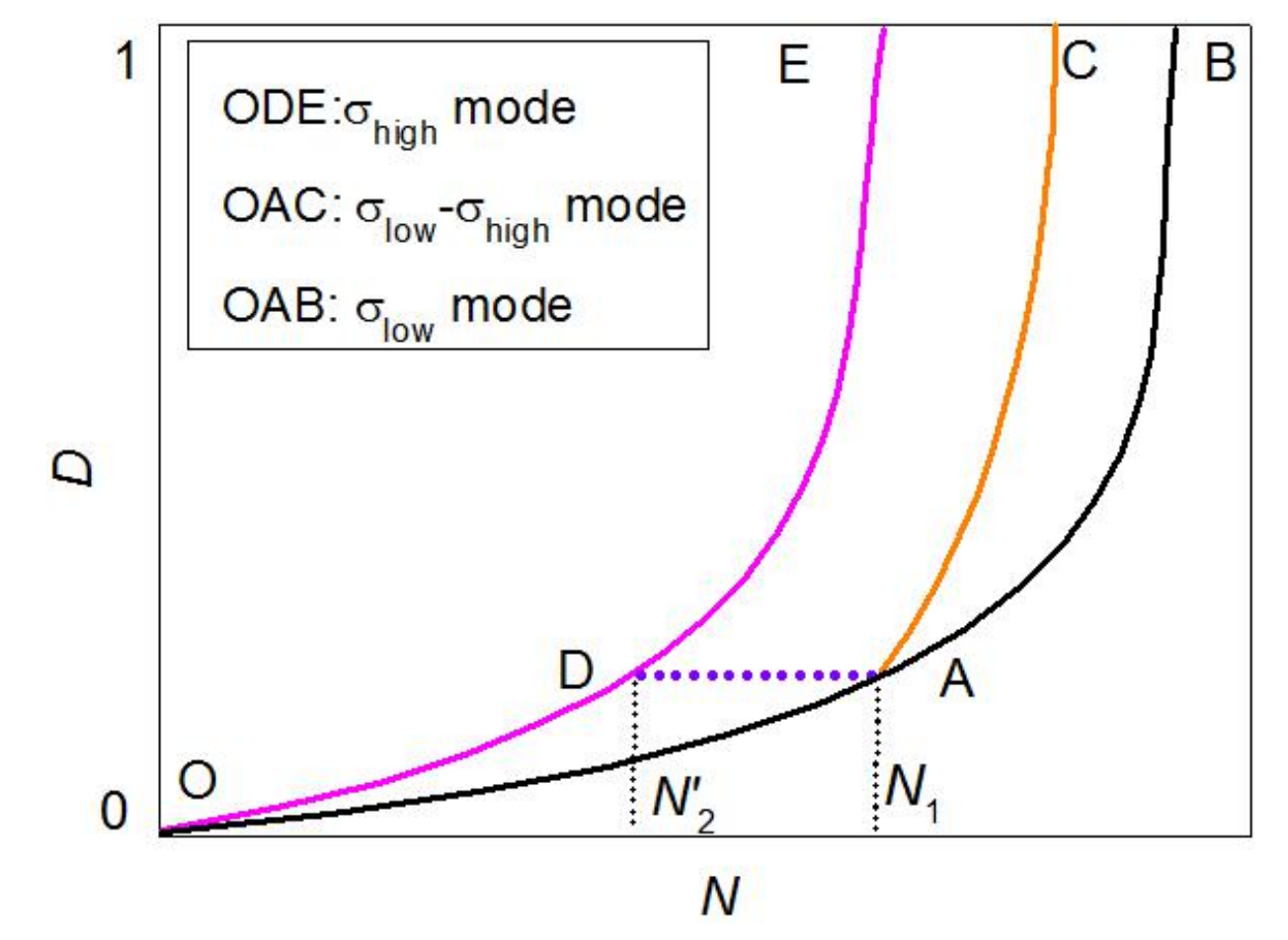
D curves

Loading sequence effect on NLFDA

- The N_2/N_{f2} of $\sigma_{low}-\sigma_{high}$ and $\sigma_{high}-\sigma_{low}$ modes are **different**, which indicates that the **NLFDA is affected by loading sequence**.



N_2/N_{f2} of different modes



Damage accumulation path

Loading interaction effect on NLFDA

- According to the **equivalence of fatigue damage**, the damage caused by σ_1 for N_1 cycles should be equal to that caused by σ_2 for N_2 cycles.
- However, the path **AC is not parallel to DE**, which indicates the **NLFDA is affected by loading interaction**.

NLFDA Model Establishment

- The **loading sequence factor (ω)** is defined as $(\sigma_1/\sigma_2)^\alpha$. The **loading interaction factor (γ)** is defined as $(1-\alpha_2)/(1-\alpha_1)$.
- According to the **damage equivalence criterion**, the NLFDA model is established based on the Chabaoche fatigue damage model.

$$D_1 = 1 - [1 - (N_1/N_{f1})^{1/(1-\alpha_1)}]^{1/(1+\beta)} = 1 - [1 - (N_2/N_{f2})^{\omega/(1-\alpha_2)}]^{1/(1+\beta)}$$

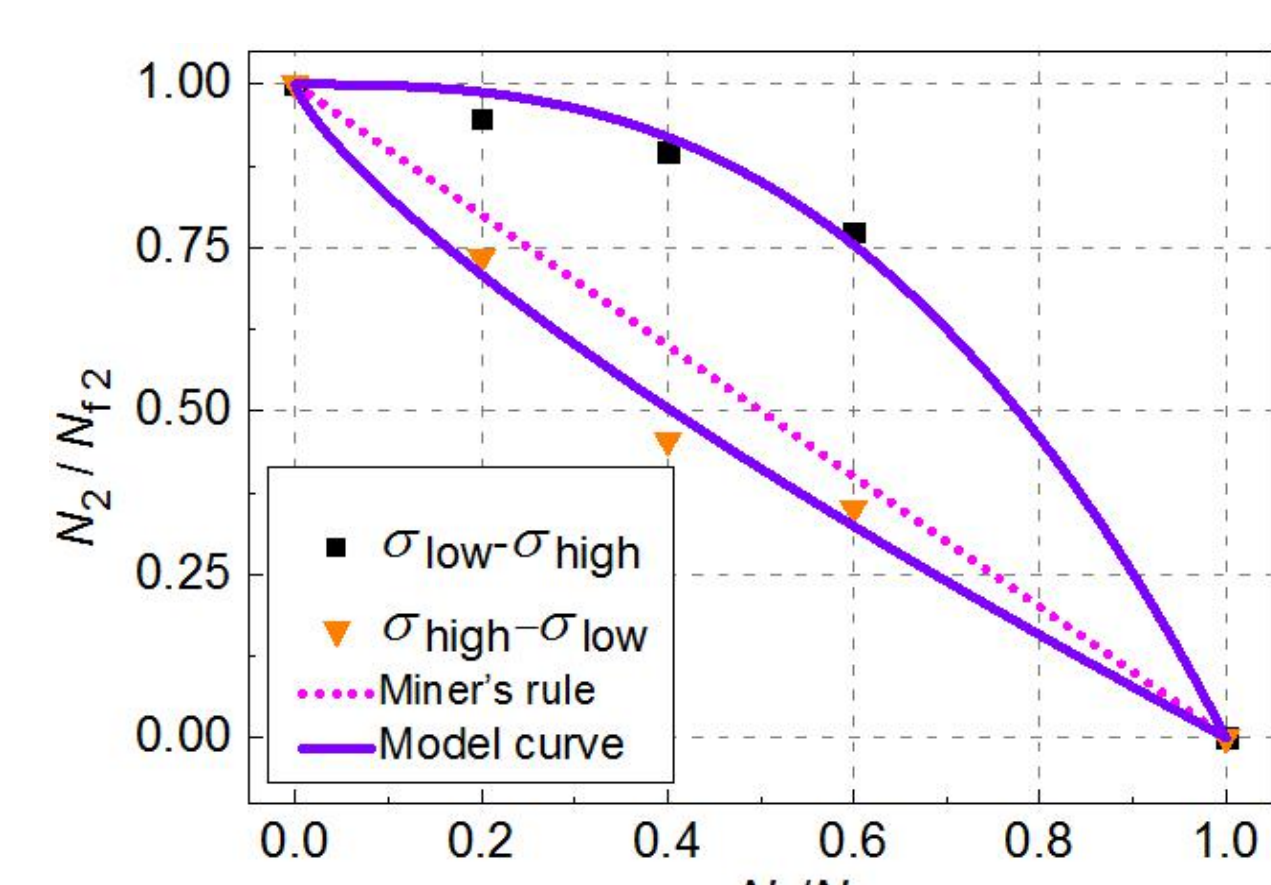
$$\Rightarrow N_2/N_{f2} = 1 - (N_1/N_{f1})^{(1-\alpha_2)/(1-\alpha_1)}$$

where α is the model parameter which depends on temperature and stress amplitude, and β is the model parameter which depends on temperature.

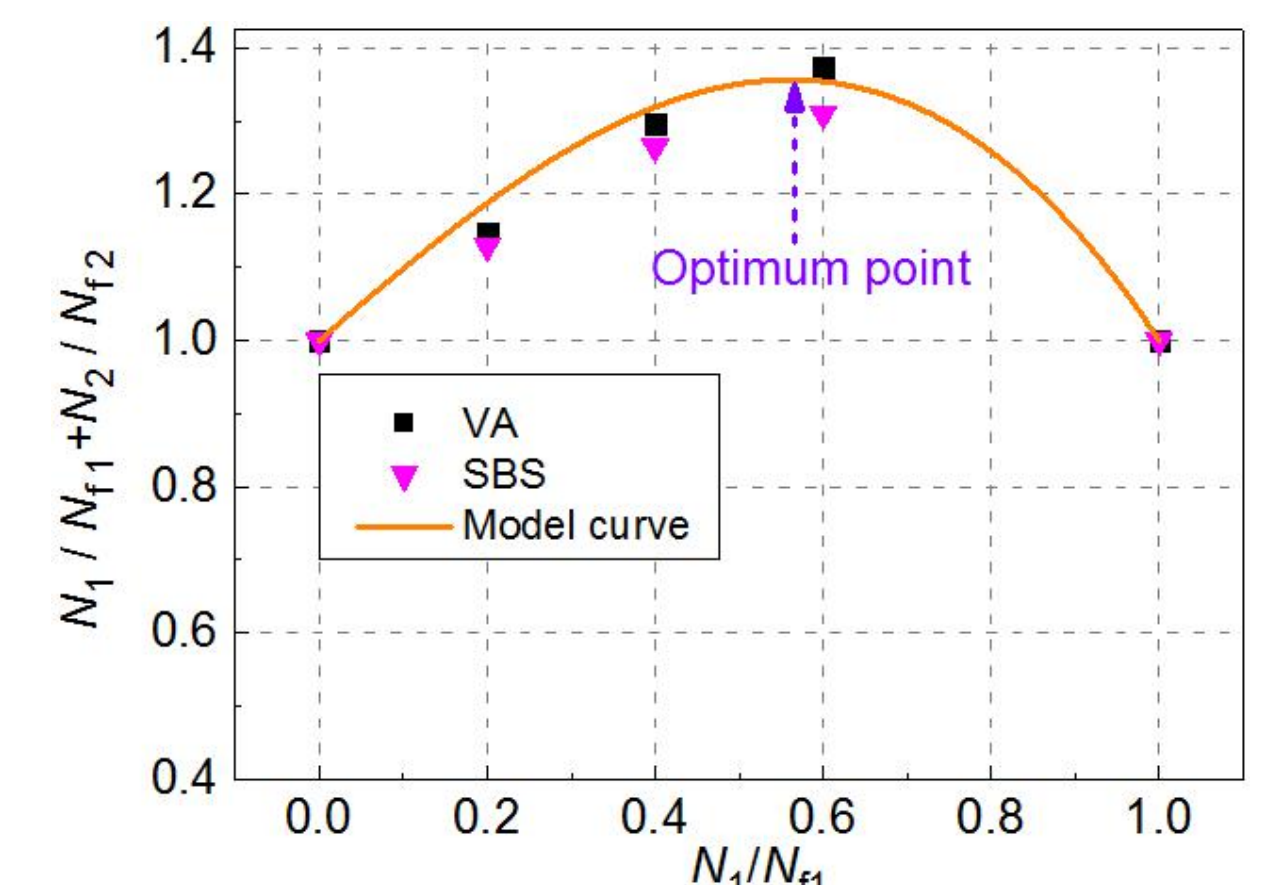
Optimum Loading Condition of Fatigue Life

- The accumulative life ratio ($N_1/N_{f1} + N_2/N_{f2}$) of $\sigma_{low}-\sigma_{high}$ mode is **greater than 1**. The $\sigma_{low}-\sigma_{high}$ mode **can extend fatigue life**. The **cumulative life ratio (R_c) model** can be established.
- The **optimum N_1/N_{f1} of $\sigma_{low}-\sigma_{high}$ model of the fatigue life of VA and SBS** can be determined, which equals to 0.53.

$$R_c = 1 - (N_1/N_{f1})^{\gamma\omega} + N_1/N_{f1} \Rightarrow N_1/N_{f1} = (\gamma\omega)^{(1-\gamma\omega)^{-1}}$$



Matching results of the NLFDA model



Optimum loading condition

Findings and Conclusions

- The **NLFDA of asphalt binder is affected by loading sequence and interaction effects**.
- The established **NLFDA model can accurately characterize the NLFDA of asphalt binder**.
- The established NLFDA model can be applied to **determine the optimum loading condition** which maximizes the **fatigue life of asphalt binder**.